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Thermal and mechanical noise in gravitational wave detectors

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UPoN, July 14th 2015

Intro GW Conclusions Newtonian Thermal Coatings Creep Virgo, a GW detector LMa Calc •1189 Ghezzano THE VIRGO COLLABORATION 5 European countries Porta a Mare (Zona Industriale) 19 laboratories - ~200 authors Riglione Oratolo

Navacchio

Montacchiello

APC Paris **ARTEMIS Nice EGO** Cascina **INFN** Firenze-Urbino **INFN** Genova **INFN Napoli INFN** Perugia **INFN** Pisa **INFN Roma La Sapienza INFN Roma Tor Vergata INFN Trento-Padova** LAL Orsay - ESPCI Paris LAPP Annecy **LKB** Paris LMA Lyon POLGRAW(Poland) **RMKI Budapest**









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Newtonian Creep Thermal Coatings Conclusions Fluctuation of local gravity

Origins

Intro GW

- Seismic fields
- Seismic point sources
- Atmosphere
- Characteristics



- Rayleigh waves are strongly attenuated with depth
- Atmospheric noise important below 10Hz. More investigations needed
- Cancellation of Newtonian Noise



• Wiener filters

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/ Thermal

Coatings

Conclusions

Creep noise

Silicate .bonding



Newtonian

Several components are under high stress

- Creep is possible
- Is it continuous or has it a shot noise like behavior?



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40 kg fused silica test mass

Main chain

Reaction chain

mirror front face

• Reduction of the problem: modal expansion

- Pendulum thermal noise separated from Mirror thermal noise: OK !
- Mode expansion not used on mirrors

The FDT

 $G_X(f) = -\frac{4k_{\rm B}T}{\omega} \operatorname{Im}[H_X(\omega)] \quad H_X(\omega) = \frac{\tilde{X}(\omega)}{\tilde{F}(\omega)}$



YAMAMOTO, ANDO, KAWABE, AND TSUBONO PHYSICAL REVIEW D 75, 082002 (2007)

K. Yamamoto, S. Otsuka, M. Ando, K. Kawabe, and K. Tsubono, Phys. Lett. A 280, 289 (2001)





Newtonian \

Creep

Thermal

Coatings

Conclusions

The coating thermal noise

- Optical Interference Coatings are used to reflect light with sub ppm absorption of light
- Transparent materials with different refractive indexes:



Creep

Thermal



Intro GW	
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Creep

1E-21

1E-22

1E-23

1E-24

1E-25

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Thermal

Coatings

Conclusions

The future of GW detectors

LIGO

- Voyager: 4km, larger mirrors cryogenic
- Cosmic Explorer: 40km, larger mirrors

Einstein Telescope

- 10 km long
- 200 kg mirrors
- 2 types of detectors
 - Room T, HF
 - Cryogenic T, LF
- Hz ^{-1/2} Lower mechanical losses Strain

FOR ALL

Factor 3 at least

Maximum distance of detection **NS-NS Binaries** ~ z = 2 BH-BH Binaries $\sim z = 17$





Coatings The amorphous materials wall

Thermal



Newtonian

Creep

- Almost all the amorphous materials have a loss angle between 10⁻⁴ and 10⁻³
- "Anomalies" are found in fused silica at room T and in amorphous Si low T



Intro GW

Conclusions

\ / Newtonian

Creep

Thermal

∫ Conclusions

Open problems in coatings noise

- Bulk losses
 - Are losses in films anisotropic?
 - Shear and bulk ?
- Interface losses
 - If any they are not dominant
- Mixing oxides
 - Why the internal friction is reduced for some particular combination of oxides?
- Annealing
 - Annealing reduces mechanical losses
 - How to avoid crystallization?
- Origin of thermal noise in amorphous materials
 - Universal law?



Coatings



K. S. GILROY and W. A. PHILLIPS PHILOSOPHICAL MAGAZINE B, 1981, VOL. 43, No. 5, 735-746

- Asymmetric Double Well Potential (ADWP)
 - 2 energy levels at $+\Delta/2$ and $-\Delta/2$, divided by a barrier of height V
 - The strain ϵ changes Δ , $-(\Delta \gamma \epsilon)/2$ τ is the typical relaxation time between the two equilibrium populations
 - The modulus defect ΔY and the time τ are:

$$\Delta Y(\Delta) = \frac{N\gamma^2}{4k_BT} \cdot \operatorname{sech}^2\left(\frac{\Delta}{2k_BT}\right) \qquad \tau = \tau_0 \operatorname{sech}\left(\frac{\Delta}{2k_BT}\right) \exp\left(\frac{V}{k_BT}\right),$$

– There are two distributions: $f(\Delta)$ and g(V)





- ∆Y≠0 for ∆~0:
 f(∆) is assumed cnst.
- g(V) exponential:
 It seems the right choice for fused silica
- For Ta₂O₅ or SiO₂ film
 g(V) comes from the curve
 loss angle vs. T

What are these relaxation mechanisms?

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Barrier height (meV)

$$\varphi(\omega) = \iint \frac{\Delta Y(\Delta)}{Y_R} \cdot \frac{\omega \tau_{V,\Delta}}{1 + (\omega \tau_{V,\Delta})^2} \cdot f(\Delta) \cdot g(V) \ d\Delta dV$$

$$\varphi(\omega) = \frac{\pi}{4} \frac{\gamma^2}{Y_R} \cdot \frac{1}{\Delta_0} \cdot \frac{n}{V_0} \cdot k_B T \cdot (\omega \tau_0)^{\frac{k_B T}{V_0}}$$





Mechanical losses

Intro GW Newtonian Creep Thermal Coatings Conclusions Conclusions Structure modeling iLM

O-2Ta

• Molecular dynamics

- Structure
- Density and elastic constants
- Vibrational properties
- Relaxations ?







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Mass

JIntro GW Newtonian Creep J Thermal

Last comments

- Among other topics
 I have not talked about:
 - Suspension Th. Noise
 - Crystalline coatings
 - Thermorefractive noise in semiconductors

Thank you for your attention

 Unsolved problems presented here

Coatings

- Newtonian noise cancellation
- ♦ Existence of creep noise
- Origin of relaxations in amorphous materials
- Thermal noise out of thermal equilibrium

Conclusions